

# Investigating the impact of surface soil moisture assimilation on state and parameter estimation in SWAT model based on the ensemble Kalman filter in upper Huai River basin

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**Abstract:** This paper investigates the impact of surface soil moisture assimilation on the estimation of both parameters and states in the Soil and Water Assessment Tool (SWAT) model using the ensemble Kalman filter (EnKF) method in upper Huai River basin. The investigation is carried out through a series of synthetic experiments and real world tests using a merged soil moisture product (ESA CCI SM) developed by the European Space Agency, and considers both the joint state-parameter updating and only state updating schemes. The synthetic experiments show that with joint state-parameter update, the estimation of model parameter SOL\_AWC (the available soil water capacity) and model states (the soil moisture in different depths) can be significantly improved by assimilating the surface soil moisture. Meanwhile, the runoff modeling for the whole catchment is also improved. With only state update, the improvement on runoff modeling shows less significance and robustness. Consistent with the synthetic experiments, the assimilation of the ESA CCI SM with joint state-parameter update shows considerable capability in the estimation of SOL\_AWC. Both the joint state-parameter update and the only state update scheme could improve the streamflow modeling although the optimal model and observation error parameters for them are quite different. However, due to the high vegetation coverage of the study basin, and the strong spatial mismatch between the satellite and the model simulated soil moisture, it is still challenging to significantly benefit the runoff estimates by assimilating the ESA CCI SM.

**Keywords:** Soil moisture; EnKF; SWAT; ESA CCI SM.

## INTRODUCTION

In hydrological simulation and forecasting, soil moisture (SM) produces significant impact on rainfall-runoff process. Over the past years, a large body of studies have been carried out to discuss the approaches to improving the estimation of SM, in turn to improve the streamflow simulation and forecast in hydrological modeling (Alvarez-Garreton et al., 2014, 2015; Brocca et al., 2012; Crosson et al., 2002; Crow and Ryu, 2009; Laiolo et al., 2015; Lunt et al., 2005; Reichle et al., 2008; Walker et al., 2001).

A promising approach to improving SM estimation and rainfall-runoff modeling is to integrate the observations of SM into hydrological modeling by the means of data assimilation (DA) techniques. This is due to the fact that the DA techniques, especially the newly developed sequential DA techniques (e.g., the ensemble Kalman filter, EnKF), provide an integrated framework to analyze all sources of uncertainties in hydrological modeling including model inputs, model parameters and model structures and the output observations (Wang et al., 2009). The SM data utilized in the assimilation can be obtained by two ways: field measurement and remote sensing observation. Aubert et al. (2003) assimilated the in-situ SM and streamflow in a lumped conceptual rainfall-runoff model using an extended Kalman filter, and demonstrated that the assimilation of SM data is particularly effective during flood events. Lee et al. (2011) assimilated the in situ soil moisture and streamflow data into a gridded Sacramento and kinematic-wave routing model and found that the prediction of soil moisture and streamflow significantly improved. Other studies on in-situ SM assimilation include Heathman et al. (2003), Lü et al. (2011) and Yu et al. (2012, 2014). However,

the field measurements can only provide SM on point scale, which usually fails to fully represent the spatial variability of SM. With the development of the remote sensing techniques since the 1990s, a large body of studies on assimilating satellite SM observations to improve hydrological modeling have been carried out from two aspects. One is mainly to evaluate the performance of SM assimilation in improving rainfall-runoff modeling by designing synthetic experiments (Chen et al., 2011; Crow and Ryu, 2009; Han et al., 2012; Reichle et al., 2008; Xie and Zhang, 2010). The other is to assimilate the satellite SM retrievals to improve the hydrological modeling (Alvarez-Garreton et al., 2014, 2015; Laiolo et al., 2015; Lievens et al., 2015). The popularity of satellite SM assimilation is due to the fact that the satellite observations could provide SM estimates with good spatial coverage and regular frequent time intervals, which is a valuable for rainfall-runoff modeling, especially on large scales and in sparsely monitored catchments.

To date, the assimilation of SM mainly focuses on improving the estimation of hydrological states and assumes that the parameters are relatively accurate and reliable in the model propagating process. This is mainly attributed to the present data quality of the remote sensing SM and its large uncertainties that are quite difficult to quantify. Besides, it can be related to the fact that the parameter estimation is more difficult than state estimation in hydrology as the relation between parameters and states are nonlinear in most hydrological models and the model parameters cannot be directly measured like states (Xie and Zhang, 2013). On the other hand, the parameters are hardly to be accurately tuned to represent the real physical coupling of the system based on the hydrological measurements (e.g., runoff measured at gauges) in

automatic calibration with certain objectives (Moradkhani et al., 2005). The biased parameters may lead to system bias in hydrological modeling (Chen et al., 2011; Troch et al., 2003), which will deteriorate the state update in the assimilation process (Moradkhani et al., 2005). Therefore, the joint state-parameter update are necessary in the assimilation process. In terms of SM assimilation, the parameters closely related to the soil property or soil water routing process can be expected to be estimated by assimilating the SM measurements considering the development of the remote sensing techniques (Barre et al., 2008; Das et al., 2014; Entekhabi et al., 2010) and the great efforts on SM retrievals in recent years (Das et al., 2011; Njoku et al., 2003). However, to our knowledge, the joint state-parameter estimation via the assimilation of the surface SM is mainly carried out through the synthetic experiments (e.g., Chen et al., 2015).

In this study, we not only use the synthetic experiments but also attempt to use the real world tests to investigate the performance of assimilating surface SM for the joint estimation of parameters and states (SM in different depths) in SWAT model using the ensemble Kalman filter (EnKF) method in the upper Huai River basin. As a comparison, we also analyze the impacts of updating only the state (SM in different depths) on rainfall-runoff modeling, where the parameters are not updated. By comparing the two cases, we want to check if the states and parameters can be estimated simultaneously by assimilating the surface SM, and if the joint state-parameter update scheme is superior to the scheme where only the state is updated.

Through the following sections of this article, the SWAT model and the EnKF approach for state and parameter estimation are described first. Then the study basin, the data utilized and the implementation of SM assimilation are introduced. After that, the results of surface SM assimilation are analyzed. Finally, the conclusions are drawn in the last section.

## METHODOLOGY

### Soil and water assessment tool (SWAT)

SWAT is a physically based basin scale distributed model developed by the USDA (United States Department of Agriculture) Agricultural Research Service (USDA-ARS) (Neitsch et al., 2011). It has been widely used in rainfall-runoff modeling in the field of hydrology in recent years (Chen et al., 2011; Xie et al., 2014). For hydrological modeling, the catchment is geographically divided into subbasins; then, each subbasin is further delineated into several Hydrological Response Units (HRUs) with the same information on land cover, soil and slope steepness. HRUs are the basic calculation units for the land phase of hydrologic cycle including the surface runoff generation, evapotranspiration, soil water routing, and groundwater generation processes.

Soil moisture plays a central role in the above processes in SWAT simulations. The water infiltrated or percolated to soil profile after surface runoff generation is redistributed using a storage routing technique with its field capacity as a threshold. The water balance equation for each soil layer can be expressed as:

$$SW'_{ly} = SW_{ly} + \Delta w_{perc,ly} - Q_{lat,ly} - E_{a,ly} \quad (1)$$

where  $SW_{ly}$  and  $SW'_{ly}$  are the soil water content (mm) at the start and end of the day respectively,  $\Delta w_{perc,ly}$  is the net percolation received in the layer  $ly$  (i.e. the percolation or infiltration from the overlying layer minus that to the next layer),  $Q_{lat,ly}$  is the

lateral flow generated from layer  $ly$ ,  $E_{a,ly}$  is the evapotranspiration drawn from the layer  $ly$ .

The percolation ( $w_{perc,ly}$ ) from layer  $ly$  is calculated as:

$$w_{perc,ly} = (SW_{ly} - FC_{ly}) \cdot (1.0 - \exp\left[\frac{-24 \cdot K_{sat,ly}}{SAT_{ly} - FC_{ly}}\right]) \quad (2)$$

where  $FC_{ly}$  is the soil water content of layer  $ly$  at field capacity (mm),  $K_{sat,ly}$  is the saturated hydraulic conductivity (mm/h),  $SAT_{ly}$  is the amount of water in layer  $ly$  when completely saturated (mm). The percolation generated from the bottom of the soil profile is the source of ground water recharge.

The lateral flow ( $Q_{lat,ly}$ ) of layer  $ly$  is calculated by:

$$Q_{lat,ly} = \frac{0.048 \cdot (SW_{ly} - FC_{ly}) \cdot K_{sat,ly} \cdot slp}{(\phi_{por,ly} - \phi_{fc,ly}) \cdot L_{hill}} \quad (3)$$

where  $slp$  is the slope steepness (m/m),  $L_{hill}$  is the hill slope length,  $\phi_{por,ly}$  is the total porosity of the soil layer (mm/mm) and  $\phi_{fc,ly}$  is the porosity of the soil layer  $ly$  filled with water when it is at field capacity.

The evapotranspiration drawn from the soil is mainly performed by soil evaporation and plant uptake. The potential evapotranspiration and the potential plant uptake are simulated first using the Penman-Monteith equation (Monteith, 1965). The plant uptake under ideal conditions is a function of the potential plant uptake and the leaf area index. The potential soil water evaporation and the ideal plant water uptake in each layer on a profile are estimated using the depth distribution function. The actual soil water evaporation and plant uptake are constrained by the available soil water of a given layer and are not allowed to be compensated by other layers. However, this deficiency can be made up by adjusting the soil compensation factor (ESCO) and the plant compensation factor (EPCO) to modify the depth distribution of the potential soil water evaporation and the ideal plant uptake.

The surface runoff, lateral flow and ground water generated on each HRU are aggregated to the main channel. SWAT incorporates a storage feature to calculate the surface runoff and lateral flow that can reach the main channel on current day, while a technique similar to the linear reservoir method is used to route the ground water to the main channel. The water routing through the channel network is realized by the variable storage routing method (Williams, 1969).

### The ensemble Kalman filter for state and parameter estimation

The Ensemble Kalman filter (EnKF) is a sequential DA approach, which was first introduced by Evensen (1994). It incorporates the Monte Carlo method to generate a state ensemble to represent the probability distribution of the state. The state forecast is then achieved by propagating the ensemble members forward in time using the model independently with a stochastic term representing the model errors (Evensen, 1994). The forecasted state ensemble  $\theta_t^f$  at time  $t$  is given by:

$$\theta_t^f = F(\theta_{t-1}^u, u_t) + w_t \quad w_t \sim N(0, r^2) \quad (4)$$

where  $F$  represents the SWAT model in this study.  $\theta_{t-1}^u$  is the updated state ensemble at time  $t-1$ . In this study, it includes the SM of four layers for all HRUs of the watershed.  $u_t$  is the mod-

el forcing input at time  $t$ , which is assumed to follow a normal distribution.  $w_t$  is the stochastic perturbation of the forecast states, which reflects the model structure error and is assumed to be normally distributed with mean 0 and covariance of  $r^2$ .

The state update is obtained by:

$$\theta_t^u = \theta_t^f + K_t[Z_t - H(\theta_t^f)] \quad (5)$$

where  $Z_t$  is the observation matrix at time  $t$ , which includes the SM observations with a stochastic perturbation being assumed to be normal distribution with mean 0 and standard deviation of  $\varepsilon$ .  $H$  is observation operator, which is used to map the model states to the observations. In the synthetic experiments,  $Z_t$  includes the surface SM of all subbasins, and  $H$  is constructed by 0 and the area proportions of HRU in subbasins as the simulated SM are on HRU level while the synthetic surface SM observations are on subbasins. In the real world test,  $Z_t$  are the surface SM on the remote sensing grids covering the whole basin, so,  $H$  is constructed by 0 and the area proportions of HRU in the grids as the simulated SM are on HRU level while the SM observations are on the grids.  $K_t$  is the Kalman gain at time  $t$ , which defines the weight of modeling and observation and is calculated by the forecast error covariance and the observation error covariance:

$$K_t = P_{ms,t} (P_{s,t} + R_{s,t})^{-1} \quad (6)$$

where  $P_{ms,t}$  is the cross error covariance between the predicted states  $\theta_t^f$  and the measurement prediction  $H(\theta_t^f)$  at time  $t$ ,  $P_{s,t}$  is the error covariance of the measurement prediction at time  $t$ ,  $R_{s,t}$  is the error covariance of the observations at time  $t$ .

The joint state-parameter updating in state augmentation technique is done by concatenating the states ( $\theta_t^f$ ) with the parameters ( $\delta_t^f$ ) in the state vector, see equation (7), and the parameter update is the same with that of the state update described in equations (5) and (6):

$$\begin{bmatrix} \theta \\ \delta \end{bmatrix}_t^u = \begin{bmatrix} \theta \\ \delta \end{bmatrix}_t^f + K_t^* (Z_t - H^* \begin{bmatrix} \theta \\ \delta \end{bmatrix}_t^f) \quad (7)$$

Since the parameters ( $\delta_t^f$ ) are not observed, the observation operator for the joint state-parameter updating is:

$$H^* = \begin{bmatrix} H & 0 \end{bmatrix} \quad (8)$$

$K_t^*$  is the Kalman gain for joint state-parameter update. Its calculation is similar to the Kalman gain ( $K_t$ ) in equation (6) but with  $P_{ms,t}$  changing to the cross error covariance between the predicted states and parameters ( $[[\theta \ \delta]_t^f]^T$ ) and the measurement prediction  $H(\theta_t^f)$  at time  $t$ .

It is worth noting that the joint state-parameter updating requires an evolution of the parameters to avoid ensemble shrinkage and filter degeneracy. In this study, the conditional covariance inflation method (Aksoy et al., 2006) is adopted as described by:

$$\begin{aligned} \delta_t^f &= \delta_{t-1}^u & Var(\delta_{t-1}^u) &\geq T \\ \delta_t^f &= \delta_{t-1}^u + v_t & Var(\delta_{t-1}^u) &\leq T, \quad v_t \sim N(0, T - Var(\delta_{t-1}^u)) \end{aligned} \quad (9)$$

where  $\delta_t^f$  is the forecast parameter ensemble at time  $t$  and  $\delta_{t-1}^u$

is the updated parameter ensemble at time  $t-1$ .  $T$  is the prescribed threshold set as the initial variance multiplied by a scaling factor  $\gamma$  in this study. Considering that model blow-up commonly occurred in the assimilation process due to over updating to the parameters, a smoothing factor  $\beta$  (between 0 and 1.0) is applied to dampen the rapid temporal variation of parameters (Yang and Delsole, 2009):

$$\delta_t^f = (1-\beta)\delta_{t-1}^u + \beta\delta_{t-1}^f \quad (10)$$

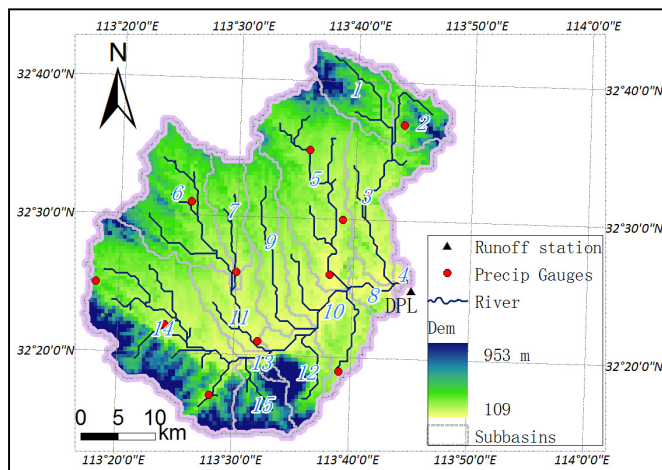
where  $\beta = 0$  reflects that there is no smoothing in the parameter updating process, the larger value of  $\beta$  indicates the stronger smoothing on parameter update.

## STUDY AREA AND DATA USED

The study catchment is located in the upper Huai River basin within  $113^\circ 15'E \sim 113^\circ 55'E$  and  $32^\circ 10'N \sim 32^\circ 45'N$  in China (Figure 1). It covers an area of about  $1640 \text{ km}^2$  with the elevation ranging from 109 m to 953 m. The basin is located in the transition zone between the northern subtropical and the warm temperate zones. Average annual precipitation is about 900 mm, of which 50% to 80% falls during June to September. The dominant land cover is rice (56%) and forest (22%). Sandy loams and silt loams are the main soil types.

The SWAT model requires the meteorological forcing data and the underlying land surface data. The meteorological data are the precipitation, maximum/minimum air temperature, solar radiation, wind speed and relative humidity. The precipitation is provided by 12 local rainfall gauges in the basin (Figure 1). Other five meteorological data above are collected from Xinyang meteorological station near the basin. The land surface data includes the digital elevation data (DEM), soil category and the land cover data. The DEM data is downloaded from the Shuttle Radar Topography Mission (SRTM) with a spatial resolution of 90 m (<http://datamirror.csdb.cn/index.jsp>). The land use data is resampled from a year-1995 land use map at a scale of 1:210000 provided by the government of Xinyang city. The soil data is resampled from a soil map at a scale of 1:100000 collected from Soil Handbook of Henan province. According to this handbook, the soil of this basin can be classified into 5 categories, of which the soil texture and the corresponding USDA (United States Department of Agriculture) classification as well as the area proportions are given in Table 1. Based on the above data sets, the catchment is divided into 15 subbasins. The subbasins are further divided into 55 HRUs. Besides, the soil on profile is divided into four layers (0–50 mm, 50–200 mm, 200–400 mm and 400–800 mm) from top to bottom, except for Cugutu with two layers (0–50 mm, 50–200 mm).

The ESA CCI SM product was developed in the Climate Change Initiative (CCI) projects by the European Space Agency (ESA). It combines the soil moisture retrievals from six passive (SMMR, SSM/I, TMI, AMSR2, AMSR-E and Windsat) and two active (ERS AMI and ASCAT) microwave sensors into a global data set spanning over 30 years from 1978 to 2014 (product version 02.2). The ESA CCI SM product consists of three surface SM datasets: the active, passive and combined product. The active and passive datasets were created by fusing scatterometer and radiometer SM products respectively, while the combined product is a merged product of both the active and passive products. We use the combined ESA CCI SM product in this study, which is downloaded from



**Fig. 1.** The upper Huai River catchment. Note: the number 1 to 15 represents the subbasin number. DPL means Dapoling runoff station.

(<http://www.esa-soilmoisture-cci.org/node/145>) with a spatial resolution of  $0.25^\circ$  and a temporal resolution of 1 day with the reference time at 0:00 UTC.

## IMPLEMENTATION OF SURFACE SOIL MOISTURE ASSIMILATION

The uncertainties of hydrological modeling are included in the meteorological forcing inputs, model parameters and model structures. These uncertainties are quantified by the variance of the ensemble members in EnKF, and each ensemble member is generated by the perturbations on model forcing inputs (including the precipitation and the minimum and maximum temperature), sensitive model parameters and the predicted SM presented in Table 2. Precipitation at each site is perturbed with a multiplicative error (Clark et al., 2008; Xie and Zhang, 2010) to avoid negative values after perturbation. The standard deviations (STD) of the multiplicative error ( $\sigma_p$ ) reflect the instrument error and the error of the spatial representativeness of the rainfall gauges. Both the maximum and minimum temperature are perturbed by an additive error with a STD of  $1.0^\circ\text{C}$ , which is also adopted by Chen et al. (2011). The model states (the SM at 4 layers) are perturbed using Gaussian multiplicative error to account for the uncertainties in model structures. This small error design of 0.01 is to avoid rapid changes of soil water content between continuous time steps. Besides, it prevents the spurious correlations between the surface SM and the SM in depths, especially when the model has weak vertical coupling in soil water routing process. In addition, the parameters sensitive to SM are assumed to be uniformly distributed within their potential value ranges. Regarding to the uncertainty of the surface SM observation, an additive error of 0.04 mm/mm is adopted (Crow and Wood,

2003; Reichle et al., 2008). In the conditional covariance inflation approach, the scaling factor  $\gamma$  used to determine the threshold  $T$  is set to 0.01 and the smoothing factor  $\beta$  is assumed 0.8 (Yang and Delsole, 2009) to dampen the rapid temporal variation of parameters during parameter evolution process.

In the synthetic experiment, three sets of data are generated, i.e., the synthetic truth run, ensemble open loop (EnOL) run and EnKF run. The synthetic truth is one realization of SWAT model running by adding perturbations on model inputs and model parameters. The synthetic surface SM observations (0–50 mm) on subbasins are generated by adding the observation errors (Table 2) to the synthetic “true” subbasin average SM from the assumed true model running process. The EnOL run is an ensemble running of SWAT model with perturbations on model inputs, model parameters and model states (SM in different depths) described in Table 2. The EnKF run is an ensemble running of SWAT model with the same error assumption to EnOL, but with the integration of the synthetic surface SM observations during the model propagation process. Here, two schemes are considered in the EnKF run: (1) the EnKF\_SP, where both the SM and parameters sensitive to SM are simultaneously updated via EnKF method; (2) the EnKF\_S, where only the SM are updated after the bias caused by the parameters is removed by the joint state-parameter update scheme of the first 200 days. The ensemble size of EnOL and EnKF is set as 100 considering the requirement on the accuracy and the computational burden. The performance of SM assimilation is illustrated by comparing the results of EnKF to that of EnOL based on the synthetic truth. In order to ensure the robustness of the analysis results, ten synthetic truths are generated considering the possible different performance of SM assimilation in different conditions (dry or wet situations). The model initialization is from Jan 1, 2005 to Dec 31, 2005, and the assimilation is from Jan 1, 2006 to Dec 31, 2008.

In the real world test, the combined ESA CCI SM product is assimilated. The assimilation of satellite soil moisture is a complex task, the success of which highly relies on the appropriate assumptions on the rescaling techniques and the model and observation errors (Massari et al., 2015). Here, the cumulative distribution function (CDF) matching method (Reichle and Koster, 2004) is used with 3 year training window (from 2003-1-1 to 2005-1-1) to remove the biases between the satellite SM and the model simulated SM before assimilation, which have been proved to be effective in many previous researches (e.g., Alvarez-Garreton et al., 2014). Then the biased removed ESA CCI SM data are assimilated for the period from Jan 1, 2006 to Dec 31, 2008.

In terms of the error set for model and observations, we will assume an appropriate value first, and then attempt to explore the sensitivity of the assimilation results to the error parameters of model and observations. For the model error, a Gaussian multiplicative perturbation with the standard deviation ( $\sigma_p$ ) of 0.4 is put on the precipitation; the parameters sensitive to SM (i.e., SOL\_AWC for different soil types) are perturbed by a

**Table 1.** Soil classification and its physical properties for the study basin.

| Chinese soil type | Clay (%) | Silt (%) | Sand (%) | Rock (%) | USDA soil texture | Area coverage (%) | $\Phi_{por}$ (mm/mm) | $\Phi_{wp}$ (mm/mm) |
|-------------------|----------|----------|----------|----------|-------------------|-------------------|----------------------|---------------------|
| Cugutu            | 7.05     | 34       | 35.9     | 23.1     | Sandy loam        | 40.6              | 0.38                 | 0.05                |
| Huanghetu         | 23.43    | 65.1     | 11.5     | 0        | Silt loam         | 23.64             | 0.42                 | 0.14                |
| Huangzongrang     | 17.03    | 39.4     | 43.6     | 0        | Loam              | 10.18             | 0.39                 | 0.11                |
| Huichaotu         | 12.86    | 51.8     | 35.3     | 0        | Silt loam         | 1.01              | 0.38                 | 0.08                |
| Shuidaotu         | 16.46    | 71       | 12.5     | 0        | Silt loam         | 24.57             | 0.41                 | 0.11                |

**Table 2.** Generation of perturbations on model and observations for each ensemble member.

| Variables            | Error distribution       | Mean | Standard deviation                     | Bound                                  |
|----------------------|--------------------------|------|----------------------------------------|----------------------------------------|
| recipitation         | Gaussian, Multiplicative | 1    | 0.2                                    | (0, -)                                 |
| Max temp             | Gaussian, Additive       | 0    | 1.0 (°C)                               | –                                      |
| Min temp             | Gaussian, Additive       | 0    | 1.0 (°C)                               | –                                      |
| Predicted SM         | Gaussian, multiplicative | 1    | 0.01                                   | (0, -)                                 |
| Parameters (SOL_AWC) | Uniform distribution     | –    | –                                      | given in Section Parameter sensitivity |
| Observed SM          | Gaussian, Additive       | 0    | 0.04 (m <sup>3</sup> /m <sup>3</sup> ) | (0, -)                                 |

Note: "Max", "Min" and "temp" means maximum, minimum, and temperature respectively.

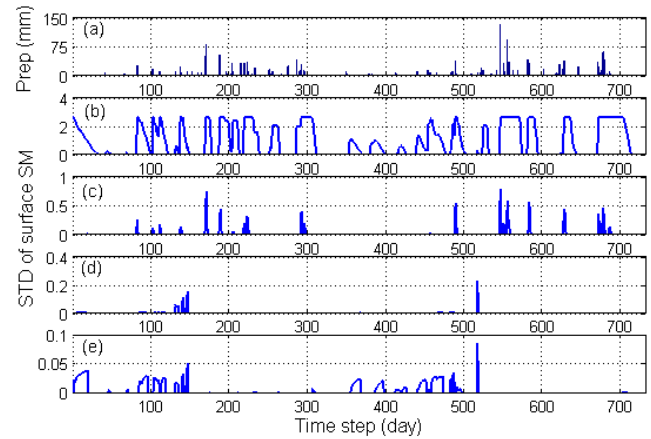
Gaussian additive noise with the standard deviation of 0.05 mm/mm to ensure that the perturbed parameters stay in physical domain detailed in the Section of Parameter sensitivity. Besides, the error set for model inputs of the maximum and minimum temperatures and the model states are identical to that of the synthetic experiment. For the observation error, an upper bound of the rescaled ESA CCI SM error is firstly determined, and a scaling factor (SF) of 80% is firstly attempted (Alvarez-Garretón et al., 2014). Similarly, the two schemes (EnKF\_SP and EnKF\_S) in the EnKF run are considered. In EnKF\_SP both the parameters and SM in different depths are updated. However, in EnKF\_S only the SM in different depths are updated while the perturbed parameters with Gaussian distribution remains unchanged.

## RESULTS

### Parameter sensitivity analysis

Theoretically, the assimilation is only effective when there is a strong correlation between the model states being updated and the observations being assimilated (Xie and Zhang, 2013). This principle is also appropriate for parameter estimation, which means that it is impossible to correct parameters that cause smaller scale errors in the predicted observation equivalent of the model states than can be observed (Smith, 2010). Therefore, it is crucial to evaluate the sensitivity of the given parameters to the measurement model predictions. Here, four parameters related to soil property and soil water routing processes are pre-selected and described in Table 3. The sensitivity analysis of the four parameters to the surface SM is conducted based on the theory of Latin Hypercube (McKay et al., 1979) and One-factor-At-a-Time (LH-OAT) sampling approach (Morris, 1991). For each parameter, an ensemble of 100 members are sampled from its value range (Table 3) using a stratified sampling method at the start of modeling. Other remaining parameters are kept at their calibrated values. After running the model, the corresponding standard deviation (STD) of the surface SM for 100 members is calculated. The larger STD values (reflect the large ensemble spread) of the surface SM ensemble indicates higher sensitivity of the corresponding parameter. Figure 2 demonstrates the sensitivity results of the four parameters on HRU-1 as an example. It is clear that SOL\_AWC is the most sensitive among the four parameters. The other three parameters only present certain sensitivity occasionally: the saturated hydraulic conductivity ( $K_{sat}$ ) is sensitive only during rainy periods,

while the soil evaporation compensation factor (ESCO) and the plant uptake compensation factor (EPCO) are only sensitive in dry periods. Therefore, only SOL\_AWC is finally selected and will be updated in this study. When taking samples of SOL\_AWC for doing the synthetic experiment or perturbing SOL\_AWC for doing the real world test, we should ensure that the value falls within its physical domain. As SOL\_AWC is the difference between field capacity  $\Phi_{fc}$  and permanent wilting point  $\Phi_{wp}$ , and  $\Phi_{fc}$  is less than the total soil porosity  $\Phi_{por}$ , therefore, the physical domain of SOL\_AWC should be between zero and  $\Phi_{por} - \Phi_{wp}$ , that is, (0, 0.33), (0, 0.28), (0, 0.28), (0, 0.3) and (0, 0.3) for Cugutu, Huanghetu, Huangzongrang, Huichaotu and Shuidaotu, respectively, according to the values of  $\Phi_{por}$  and  $\Phi_{wp}$  given in Table 1.



**Fig. 2.** Variations of the catchment average precipitation (Prep) and the standard deviation (STD) of surface soil moisture (SM) for four parameters (Table 3) on HRU-1 from 1994-1-1 to 1995-12-31. (a) precipitation (b) SOL\_AWC (c)  $K_{sat}$  (d) ESCO (e) EPCO.

### Results for the synthetic experiments

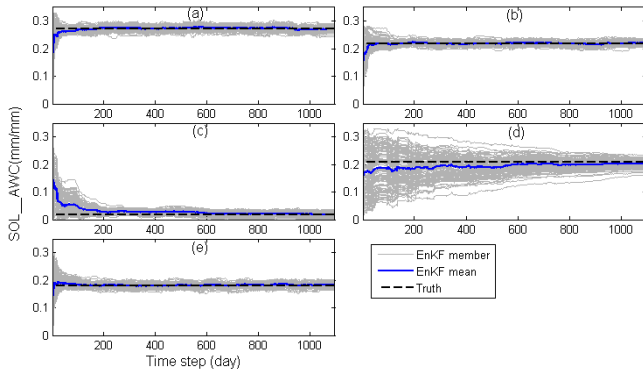
#### Parameter and state estimation

Figure 3 shows the assimilation process of SOL\_AWC for the 5 types of soil in one experiment randomly chosen from the ten experiments. It is found that the SOL\_AWC for 4 types of soil (except for Huichaotu, Figure 3(d)) can be accurately estimated by assimilating the synthetic surface SM observations.

**Table 3.** Parameters closely related to soil moisture in SWAT.

| Parameter | Units   | Description                                                                                                                                                          | Value range |
|-----------|---------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|
| SOL_AWC   | mm /mm  | Available water capacity of the soil, which is calculated by subtracting the fraction of water present at permanentwilting point from that present at field capacity | (0.01, 1.0) |
| $K_{sat}$ | mm/hour | Saturated hydraulic conductivity                                                                                                                                     | (0.0, 250)  |
| ESCO      | –       | Soil evaporation compensation factor                                                                                                                                 | (0.01, 1.0) |
| EPCO      | –       | Plant uptake compensation factor                                                                                                                                     | (0.01, 1.0) |

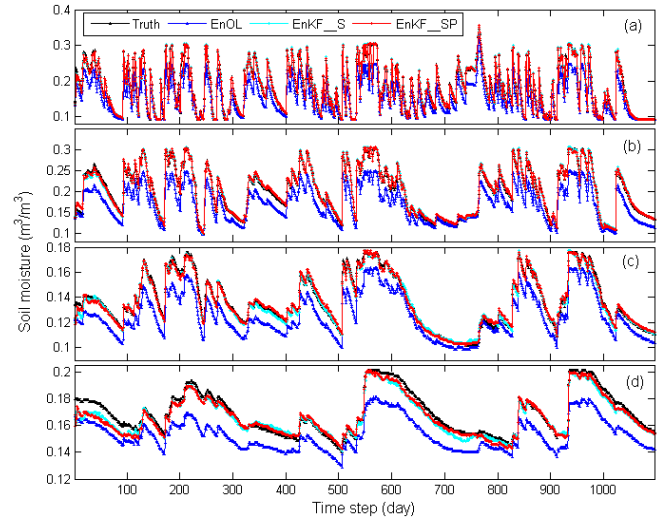




**Fig. 3.** Estimation of the parameter SOL\_AWC for the 5 types of soil from 2006-1-1 to 2008-12-31 by assimilating the synthetic surface soil moisture observations. (a) Cugutu (b) Huanghetu (c) Huangzongrang (d) Huichaotu (e) Shuidaotu.

Although there is a bias (i.e., a difference between the ensemble mean and the synthetic truth) at the start of assimilation, after about 200 days at maximum, all the ensemble members of SOL\_AWC converge to the truth and the ensemble mean matches the truth well. This indicates the significant capability of surface SM assimilation to eliminate parameter bias and improve the estimation of SOL\_AWC. The non-convergence and underestimation of SOL\_AWC for soil Huichaotu is partly caused by its little area proportion (1.01%) in the study basin. The change of SOL\_AWC for Huichaotu cannot cause large difference in the surface SM modeling on subbasins, thus its estimation by assimilating the surface SM on subbasin scale contains certain difficulty. The results are similar for other nine experiments.

Figure 4 provides the catchment area average SM of four layers (0–50 mm, 50–200 mm, 200–400 mm and 400–800 mm) from top to bottom in EnOL, EnKF\_SP, EnKF\_S and the synthetic truth, which are obtained from the same experiment mentioned above. The SM estimated by EnKF\_SP is significantly improved compared with that by EnOL, especially for the upper two layers, as it significantly approaches the synthetic truth during the assimilation process. This can be illustrated from the decrease of the root mean square error (RMSE) by EnKF\_SP compared with that by EnOL (Table 4). Nevertheless, it seems that the effects of EnKF\_SP on SM estimation show a decreasing trend with the increase of soil depth, which can be revealed from the decreasing degree of RMSE reduction in Table 4. This decreased efficiency is certainly influenced by the weak vertical coupling in SWAT model (Chen et al., 2011), which weakens the correlation between the surface SM and the SM in depths and deteriorates the SM update in deep layers in the assimilation. Besides, it can be seen in Figure 4 that the EnKF\_S obtains similar performance on SM estimation to EnKF\_SP, which indicates that the joint state-parameter update after 200 days does not make large difference to that with only state update on SM estimation. This is because the parameter SOL\_AWC has gradually converged to stable values during the first 200 days by joint state-parameter update in EnKF\_S. It makes the observations having little effect on the parameters after 200 days in EnKF\_SP. Thus, the EnKF\_S and EnKF\_SP show similar influence on SM estimation. However, in terms of the RMSE in Table 4, the EnKF\_S produces a little inferior impacts on the SM estimation of the fourth layer compared with that of the EnKF\_SP (Table 4). This might relate to the lack of the possible temporal evolution of the model parameters in



**Fig. 4.** The catchment area average soil moisture for the four layers from top to bottom estimated in the EnKF and EnOL from 2006-1-1 to 2008-12-31. (a) the first layer (0–50 mm), (b) the second layer (50–200 mm), (c) the third layer (200–400 mm) and (d) the forth layer (400–800 mm).

**Table 4.** RMSE of the catchment area average soil moisture obtained by EnOL, EnKF\_S and EnKF\_SP in the synthetic experiment (based on the data for the whole data assimilation period except for its first 200 days).

| RMSE (m <sup>3</sup> /m <sup>3</sup> ) | Layer 1 | Layer 2 | Layer 3 | Layer 4 |
|----------------------------------------|---------|---------|---------|---------|
| EnOL                                   | 0.0323  | 0.0353  | 0.0125  | 0.0175  |
| EnKF_S                                 | 0.0025  | 0.0031  | 0.0021  | 0.0038  |
| EnKF_SP                                | 0.0022  | 0.0032  | 0.0020  | 0.0029  |

Note: Layer 1, Layer 2, Layer 3 and Layer 4 represent the first (0–50 mm), second (50–200 mm), third (200–400 mm) and the forth layer (400–800 mm) respectively.

EnKF\_S as the parameters remain unchanged after 200 days (Moradkhani et al., 2005).

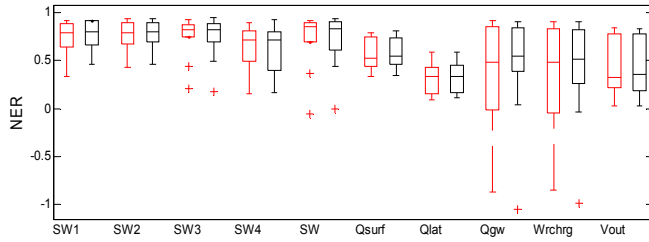
#### Effectiveness of data assimilation on rainfall-runoff modeling

The improvement of SM estimation can be expected to improve the rainfall-runoff simulation and prediction (Alvarez-Garretón et al., 2014, 2015; Brocca et al., 2012). In order to analyze the performance of surface SM assimilation on rainfall-runoff modelling, the normalized error reduction of RMSE (NER) is used:

$$NER = 1.0 - \frac{RMSE_{EnKF}}{RMSE_{EnOL}} \quad (11)$$

where  $RMSE_{EnKF}$  and  $RMSE_{EnOL}$  are the RMSE of the EnKF and EnOL mean based on the synthetic truth. The larger values of NER indicate the relatively better performance of EnKF.

Figure 5 provides the NER of the ensemble average states and flux (Table 5) for the ten synthetic experiments. It can be seen that the total runoff at the catchment outlet ( $V_{out}$ ) is considerably improved by the EnKF\_SP and EnKF\_S in the soil moisture assimilation. It seems that the  $V_{out}$  obtained by EnKF\_SP has a little better estimation than that by EnKF\_S as it obtains a bit higher median value of NER. The improvement of the total runoff is contributed by the improvement of the three



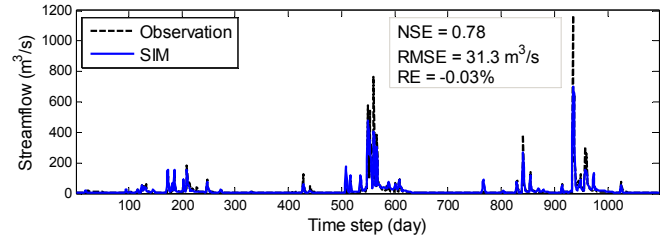
**Fig. 5.** NER (equation 11) of the EnKF\_S (red box) and EnKF\_SP (black box) ensemble averaged variables (Table 5) for the ten synthetic experiments (based on the data for the whole data assimilation period except for its first 200 days). The upper limb, lower limb and the red or black line in the box represent the upper quartile (here, represented by  $h1$ ), lower quartile (represented by  $h2$ ) and the median value of NER for the ten experiments. The dotted line stretched from the box indicates the range of  $h1-1.5(h2-h1)$  and  $h2+1.5(h2-h1)$ , while the red “+” is the strange values beyond this range.

different streamflow components including the surface runoff ( $Q_{surf}$ ), lateral flow ( $Q_{lat}$ ) and ground water ( $Q_{gw}$ ), in which  $Q_{surf}$  and  $Q_{gw}$  take the major part (about 80%) of the total runoff. The surface runoff improvement is caused by the improved SM on profile, which obtains a large degree of improvement by surface SM assimilation. The ground water primarily benefits from the improvement of the soil water recharge ( $w_{rchrg}$ ) to the shallow and deep aquifers.  $w_{rchrg}$  is the only source of ground water, which is influenced by the improvement of the soil water distribution on profile and the field water capacity (equation 2) that is controlled by SOL\_AWC. Compared to the EnKF\_SP, the worse and less robust performance of EnKF\_S on ground water resulted from the bad performance of that on  $w_{rchrg}$ , which also contribute the less significant improvement of the total runoff. This unsatisfactory performance of EnKF\_S might be related to the fact that the parameter ensemble of SOL\_AWC will not be propagated and corrected after 200 days, which might make the lack consideration of the possible temporal evolution of the model parameters in the model propagating process (Moradkhani et al., 2005). Overall, the EnKF\_SP outperforms the EnKF\_S in both the improvement level and stability of the rainfall-runoff process by the surface soil moisture assimilation. This also indicates the importance of the joint state-parameter update in soil moisture assimilation.

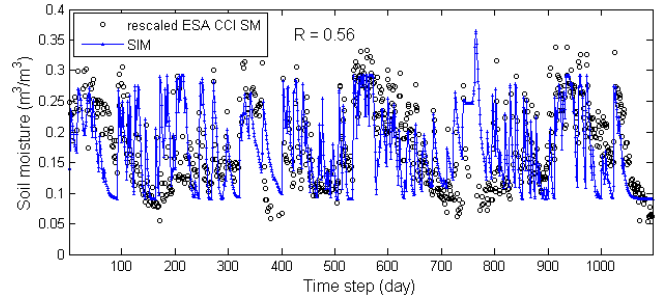
## Results for the real world tests

### Model calibration and validation

The model is calibrated using the daily runoff records from Jan 1, 2002 to Dec 31, 2005 observed at the basin outlet (Dapoling station, Figure 1). The parameter optimization is achieved by a combination of auto calibration using the Sequential Uncertainty Fitting (SUFI2) (Abbaspour et al., 2004) with the Nash-Sutcliffe coefficient of efficiency (NSE,



**Fig. 6.** Validation of streamflow at Dapoling station from 2006-1-1 to 2008-12-31.



**Fig. 7.** The model simulated soil moisture and rescaled ESA CCI SM on catchment scale from 2006-1-1 to 2008-12-31.

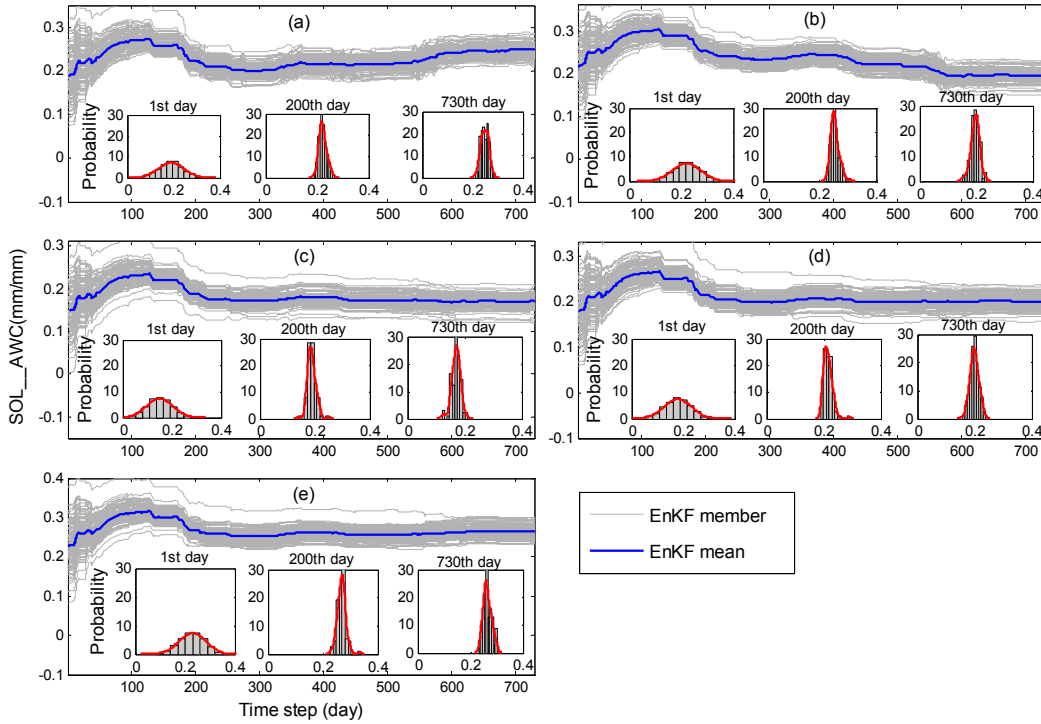
Nash and Sutcliffe, 1970) as the objective criteria and the manual fine-tuning method. The NSE, the root mean square error (RMSE) and the relative error ( $RE = (1.0 - \text{sum}(\text{SIM})/\text{sum}(\text{OBS})) * 100\%$ , where  $\text{sum}(\text{SIM})$  and  $\text{sum}(\text{OBS})$  represent the summarized value of the simulated and the observed streamflow series for the whole calculation period separately) at Dapoling station for the calibration period are 0.74, 44.38  $\text{m}^3/\text{s}$  and 2.43% respectively. Figure 6 shows the validation of streamflow at Dapoling station from Jan 1, 2006 to Dec 31, 2008. The NSE, RMSE and RE are 0.78, 31.3  $\text{m}^3/\text{s}$  and  $-0.03\%$  respectively for this period. The model simulated soil moisture and the rescaled ESA CCI SM on the basin in this validation period are present in Figure 7. It can be seen that the model simulated soil moisture varies more frequently than that of the ESA CCI SM. The Pearson's correlation coefficient between them is 0.56.

### Parameter estimation and validation

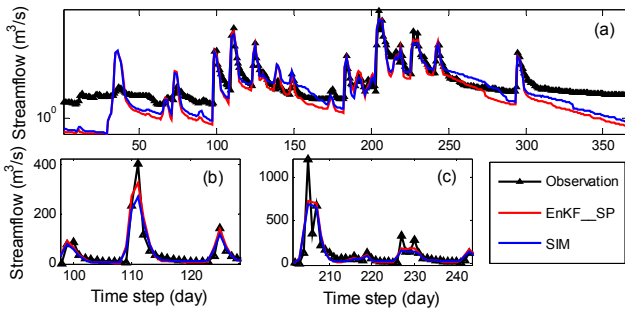
Figure 8 presents the SOL\_AWC for 5 types of soil by assimilating the combined ESA CCI SM products from Jan 1, 2006 to Dec 31, 2007 in EnKF\_SP. After about 200 days, the ensemble trajectories are nearly stable with little variations, and the ensemble samples can be approximated by a Gaussian distribution with a small standard deviation (STD). This indicates that the uncertainty of the parameter estimation can be decreased with the joint state-parameter update in EnKF\_SP. The relatively stable ensemble trajectory and the little ensemble spread

**Table 5.** The variables in SWAT model marking the rainfall-runoff process.

| Variables   | Units                 | Description                                                               |
|-------------|-----------------------|---------------------------------------------------------------------------|
| $SW_{ly}$   | mm                    | Watershed average soil water content in layer $ly$ on a given day         |
| $SW$        | mm                    | Watershed average profile soil water content on a given day               |
| $Q_{surf}$  | mm                    | Amount of surface runoff discharged to the main channel on a given day    |
| $Q_{lat}$   | mm                    | Amount of lateral flow discharged to the main channel on a given day      |
| $w_{rchrg}$ | mm                    | Amount of water entering both shallow and deep aquifers on a given day    |
| $Q_{gw}$    | mm                    | Amount of ground water flow discharged to the main channel on a given day |
| $V_{out}$   | $\text{m}^3/\text{s}$ | The volume of water flowing out of the channel during a time step         |

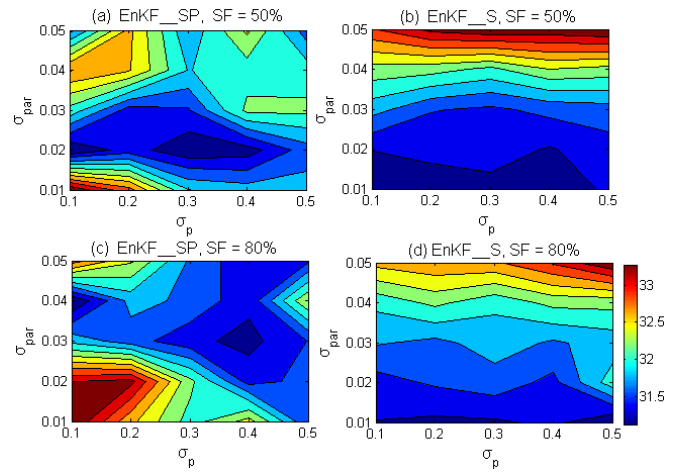


**Fig. 8.** Estimation of the parameter SOL\_AWC for the 5 types of soil from 2006-1-1 to 2007-12-31 by assimilating the combined ESA CCI SM. The histograms in each plot, fitted with the Gaussian distribution function, represent the distribution of the ensemble members at three time steps (i.e. 1st, 200th and 730th day). (a) Cugutu (b) Huanghetu (c) Huangzongrang (d) Huichaotu (e) Shuidaotu.



**Fig. 9.** The predicted streamflow using different parameter sets from 2008-1-1 to 2008-12-31.

(reflected by the STD of the parameter ensemble) imply the potential that the SOL\_AWC can be estimated probably by assimilating the combined ESA CCI SM. However, it is not sure whether the SOL\_AWC is appropriately estimated, because we cannot obtain its true value. Here, we attempt to use the streamflow measurements at the catchment outlet for parameter validation. We perform a single run of SWAT model from Jan 1, to Dec 31, 2008, using the parameter estimates from EnKF\_SP, and evaluate the predicted streamflow against the observed streamflow at the basin outlet (Dapoling station). Besides, the streamflow in the control run, i.e. the simulated streamflow using the prior calibrated parameters in the section of Model calibration and Validation, is adopted as a comparison. Figure 9 shows the predicted streamflow based on the above two parameter sets, the EnKF\_SP calibrated parameter (marked by EnKF\_SP) and the prior calibrated parameter (marked by SIM). It can be seen that the high flow obtained by the EnKF\_SP calibrated parameters is considerably improved compared to the streamflow in control run (e.g., the day around



**Fig. 10.** Contour plot of the RMSE for the outlet streamflow estimated by EnKF\_SP and EnKF\_S from Jan 1, 2006 to Dec 31, 2008, as a function of the standard deviation (STD) of the multiplicative Gaussian perturbations to the precipitation ( $\sigma_p$ ), the STD of the Gaussian perturbations on SOL\_AWC ( $\sigma_{par}$ ), and the scaling factor (SF) to the upper bound of the observation error for the rescaled ESA CCI SM.

110). However, the improvement was not obtained for the low flow. Simulated streamflow become even worse for some periods (e.g., the day over 300). For the whole period, the streamflow by EnKF\_SP only obtains a slight improvement, as the RMSE is decreased from 39.80 to 39.72  $m^3/s$  and the NSE increased from 0.77 to 0.78. Although this improvement is not significant, it still shows the capability of the satellite soil moisture assimilation in parameter optimization.



*Sensitivity of the model and observation error*

Figure 10 shows the root mean square error (RMSE) of the outlet streamflow obtained by EnKF\_SP and EnKF\_S with varying standard deviation (STD) of the Gaussian multiplicative perturbations on precipitation ( $\sigma_p$ ) from 0.1 to 0.5 along with the varying STD of the Gaussian additive perturbations on parameter SOL\_AWC ( $\sigma_{par}$ ) from 0.01 to 0.05 mm/mm. At the same time, the scaling factors (SF) to the upper bound (0.067, 0.066, 0.070 and 0.065  $\text{m}^3/\text{m}^3$  for the four remote sensing grids covering the basin) of the observation error for the rescaled ESA CCI SM are considered at 50% and 80%, while the error of the model inputs for the maximum and minimum temperature and the model states (soil moisture in different depths) remain unchanged at 1.0°C and 0.01 respectively. Figures 10 (a) and (c) show that, in terms of the RMSE for the outlet streamflow, the performance of EnKF\_SP is sensitive to both the error of SOL\_AWC ( $\sigma_{par}$ ) and the precipitation input ( $\sigma_p$ ). The optimal performance of EnKF\_SP falls in different domain of  $\sigma_p$  and  $\sigma_{par}$  with different observation errors (i.e. 50% and 80% of SF). Note that the RMSE of the simulated streamflow in the control run is 31.3  $\text{m}^3/\text{s}$  (see the section of Model calibration and Validation). The good impacts of EnKF\_SP on streamflow modeling can be obtained when  $\sigma_{par}$  is around 0.02 and  $\sigma_p$  being limited within 0.43 under the case that SF kept at 50% (Figure 10 (a)), and when SF equals 80%, the optimal  $\sigma_{par}$  and  $\sigma_p$  are around 0.03 and 0.4 respectively (Figure 10 (c)). Figures 10 (b) and (d) show that, the EnKF\_S performance is sensitive to the magnitude of the parameter perturbation ( $\sigma_{par}$ ). With the increase of  $\sigma_{par}$ , the performance of EnKF\_S on streamflow modeling becomes worse. The EnKF\_S will produce negative influence on the streamflow modeling once  $\sigma_{par}$  exceeds 0.02 when SF is kept at 50% (Figure 10(b)), and the EnKF\_S effects will be negative once  $\sigma_{par}$  exceeds 0.01 when SF is kept at 80% (Figure 10(d)). The bad performance of EnKF\_S is due to the overfitting of the model simulated soil moisture (SM) to that of the satellite soil moisture, as the large perturbation to SOL\_AWC will lead to large ensemble spread of the predicted SM. That in turn results in large forecast error covariance between the model predicted SM and the measurement predictions, which makes very large (or unreasonable) SM updates in the assimilation process. The different sensitivity of the EnKF\_SP and EnKF\_S performance to the model and observation error parameters indicate the capability of the remote sensing SM on parameter estimation. Overall, the EnKF\_SP and EnKF\_S have the capability to improve the streamflow modeling by assimilating the combined ESA CCI SM although the optimal model and observation error parameters for them are quite different. This also indicates the significance of an appropriate error assumption/quantification on the model and observations in satellite soil moisture assimilation.

**DISCUSSION AND CONCLUSIONS**

The impact of surface soil moisture assimilation on the estimation of both model parameters and model states (soil moisture in different depths) are investigated in SWAT model using the ensemble Kalman filter (EnKF) method. The investigation is based on a series of synthetic experiments and a real world test using the combined ESA CCI SM product in the upper Huai River basin. The following two schemes are considered in EnKF: (1) both the model parameter and soil moisture in different depths are updated simultaneously by assimilating the surface soil moisture (EnKF\_SP), (2) only the soil moisture in

different depths are updated by assimilating the surface soil moisture (EnKF\_S).

In the synthetic experiments, the results of EnKF\_SP indicate that the surface soil moisture assimilation with joint state-parameter update has significant capability to improve the estimation of parameter SOL\_AWC (the available soil water capacity) and soil moisture itself in different depths, even though this improvement is decreasing with the increase of soil depth. For EnKF\_S, the surface soil moisture assimilation with only state update with unbiased parameters (the parameter bias is removed by joint parameter-state update for the first 200 days) also obtains satisfactory SM estimation in different depths on soil profile. The less significant influence of EnKF\_S on the SM estimation of the fourth layer might be related to the lack of consideration for the possible temporal evolution of the parameters in EnKF\_S as the parameters remain unchanged after 200 days in the EnKF\_S based data assimilation process. In terms of the impact of surface soil moisture assimilation on the rainfall-runoff process, the performance of EnKF\_SP is relatively better and robust than that of the EnKF\_S, especially for the ground water. This also indicates the importance of both state and parameter update on the improvement of hydrological modeling in soil moisture assimilation.

In the real world tests, the assimilation of the combined ESA CCI SM by EnKF\_SP shows that it has considerable capability in the estimation of parameter SOL\_AWC. The uncertainty of SOL\_AWC (represented by the standard deviation of the parameter ensemble) is largely decreased and the ensemble trajectory remains stable after assimilating the satellite soil moisture for about 200 days. Moreover, the predicted steamflow using the parameters from EnKF\_SP is slightly better than that from the prior calibration, which also reflects the capability of the satellite soil moisture in parameter optimization. The sensitivity analysis of the EnKF\_SP and EnKF\_S performance on streamflow modeling to the model and observation errors shows that both of them have the capability to improve the streamflow modeling by assimilating the combined ESA CCI SM although the optimal model and observation error parameters for them are quite different. However, the improvement of streamflow modeling by EnKF\_SP and EnKF\_S in the combined ESA CCI SM assimilation is not significant in this study. This result can be analyzed from the following three aspects: (1) The underlying conditions of the study catchment might influence the usefulness of the combined ESA CCI SM product. The dominant land cover of this basin is rice (56%), which is usually wet and with high density of vegetation cover. This will deteriorate the data quality of the satellite soil moisture retrievals. Besides, the mountainous region takes about 30% in this basin, of which the undulating terrain might also produce bad influence on the utility of the remote sensing data. Also, Brocca et al. (2013) did not find significant improvement in the mountainous region by assimilating different soil moisture products into rainfall-runoff modeling using a simple nudging scheme. (2) The spatial mismatch between the satellite soil moisture and the model simulated soil moisture might influence the assimilation performance. The grid-based ESA CCI SM has a spatial resolution of about 25 km, which is much larger than that of the model simulated soil moisture. The coarse spatial resolution of the soil moisture observation might weaken its sensitivity to the changes of hydrological modeling, thus influence its assimilation performance. (3) The simplification on the model and observation error assumption might affect the optimality of the assimilation scheme. The model error is assumed a Gaussian additive or multiplicative distribution, and the spatial and temporal correlations of the error (e.g., the model input error for precipi-

tations) are not considered. Besides, the non-stationary error characteristics for the satellite soil moisture are also ignored in this study. Therefore, based on the knowledge that the surface soil moisture assimilation has the capability to improve the state and parameter estimates, a lot of future work needs to be done to improve the data quality of the satellite soil moisture products and their utilization by optimizing the data assimilation scheme to improve the rainfall-runoff modeling.

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## NOMENCLATURE

|                |                                                                                                   |
|----------------|---------------------------------------------------------------------------------------------------|
| SWAT           | Soil and Water Assessment Tool                                                                    |
| EnKF           | the ensemble Kalman filter method                                                                 |
| SM             | soil moisture                                                                                     |
| ESA CCI        | the soil moisture products in the Climate Change Initiative projects by the European Space Agency |
| SM             | Hydrological Response Units                                                                       |
| HRU            | standard deviation                                                                                |
| STD            | open loop                                                                                         |
| EnOL           | EnKF with only state update                                                                       |
| EnKF_S         | EnKF with joint state-parameter update                                                            |
| EnKF_SP        | simulation                                                                                        |
| SIM            | observation                                                                                       |
| OBS            | soil evaporation compensation factor                                                              |
| ESCO           | plant evaporation compensation factor                                                             |
| EPSCO          | saturated hydraulic conductivity                                                                  |
| $K_{sat}$      | available soil water capacity                                                                     |
| SOL_AWC        | fraction of water content at wilting point                                                        |
| $\Phi_{wp}$    | fraction of water content at field capacity                                                       |
| $\Phi_{fc}$    | field water capacity                                                                              |
| FC             | total soil porosity                                                                               |
| $\Phi_{por}$   | root mean square error                                                                            |
| RMSE           | normalized reduction of the root mean square error                                                |
| NER            | relative error                                                                                    |
| RE             | Nash and Sutcliffe coefficient                                                                    |
| NSE            | standard deviation of the Gaussian multiplicative perturbation on precipitation                   |
| $\sigma_p$     | standard deviation of the Gaussian additive perturbation on parameters                            |
| $\sigma_{par}$ | scaling factor to the upper bound of the soil moisture observation error                          |
| SF             | streamflow at the basin outlet                                                                    |
| $V_{out}$      | surface runoff                                                                                    |
| $Q_{surf}$     | lateral flow                                                                                      |
| $Q_{lat}$      | ground water                                                                                      |
| $Q_{gw}$       | water recharge to the shallow and deep aquifer from the bottom of soil profile                    |
| $w_{rchrg}$    |                                                                                                   |

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